

# Hydrometallurgical recovery of tin and copper from mobile phone printed circuit boards.

GDR Prométhée Scientific Days

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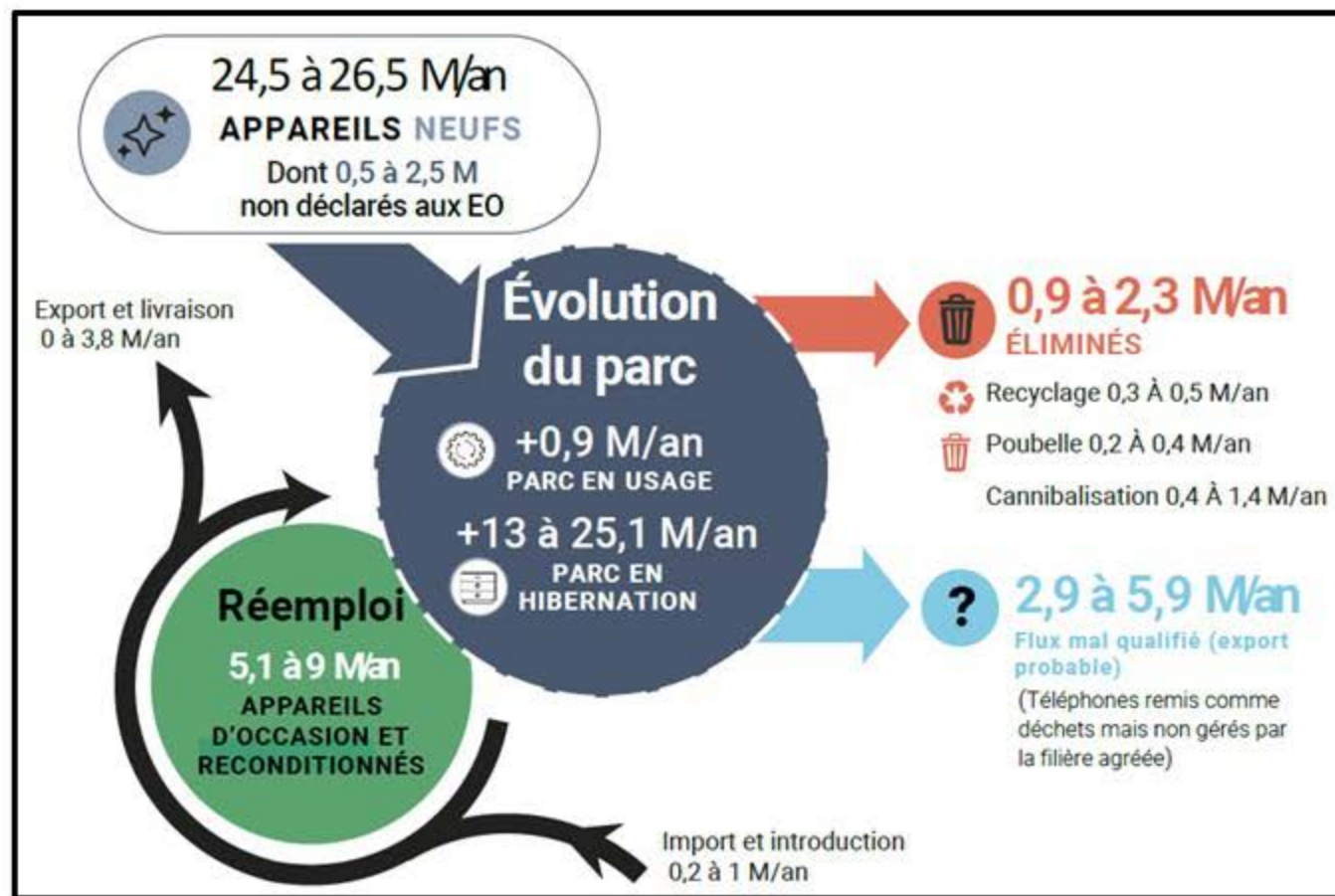
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## THYMO Project (HYdrometallurgical Treatment of MObile phones)

Over 120 millions mobile phone remain in French drawers !



Flows and fleets of mobile phones in France in 2018. [1]

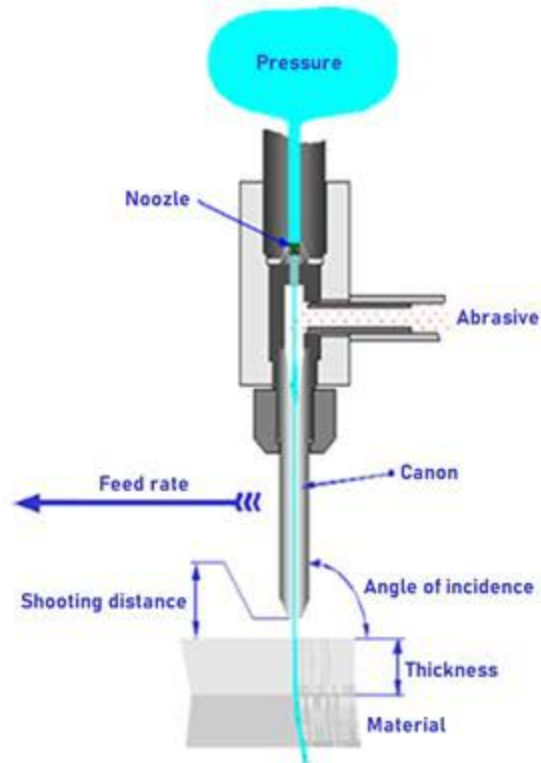
[1] Sofies and Bio Innovation Service (2019). Étude du marché et parc de téléphones portables français en vue d'augmenter durablement leur taux de collecte

- Develop an innovative process for recycling cell phone circuit boards:
  - low environmental impact
  - energy-efficient
  - enables maximum recovery of metals
  - enables the “polymer” part of the board to be recovered
- Use a significant quantity of circuit boards to obtain realistic raw material



**Collection of  
over 19000  
mobiles  
phones**

## Automated process by CRITT-TJFU



Printed circuit boards or PCBs  
Theoretical industrial rate : up to 400  
phones per minute

## Pre-treatment



PCBs from  
CRITT TJFU



Shredding to  
8 mm



Magnetic sorting  
Eddy Current

geo  
Ressources



Shredding  
(hammer mill)

Sizing < 500  $\mu$ m

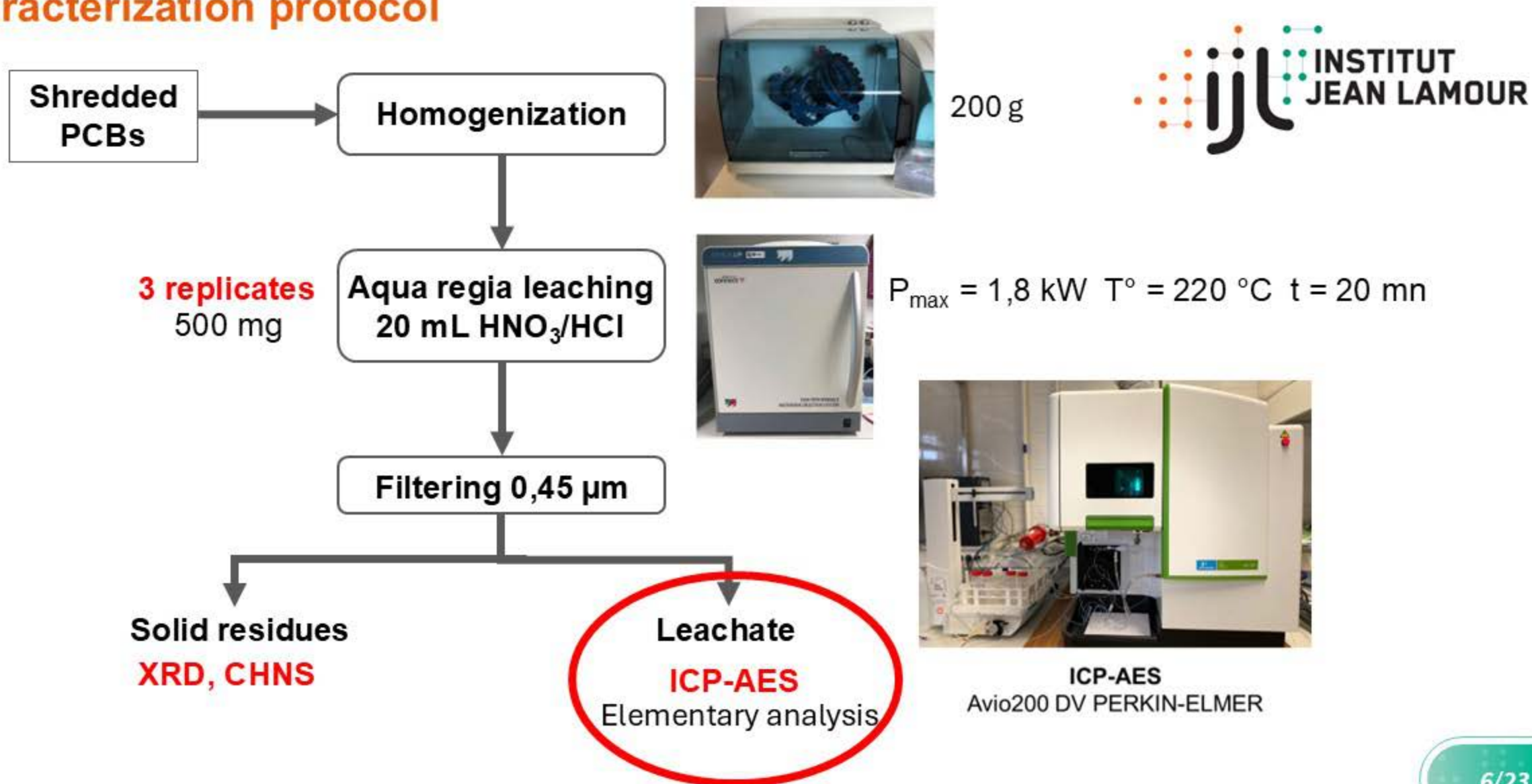


Shaking table

**Light fraction** : epoxy resin, glass fibers, aluminum

**Heavy fraction** : **metals**, ceramics ( $\text{BaSO}_4$ ,  $\text{Al}_2\text{O}_3$ )

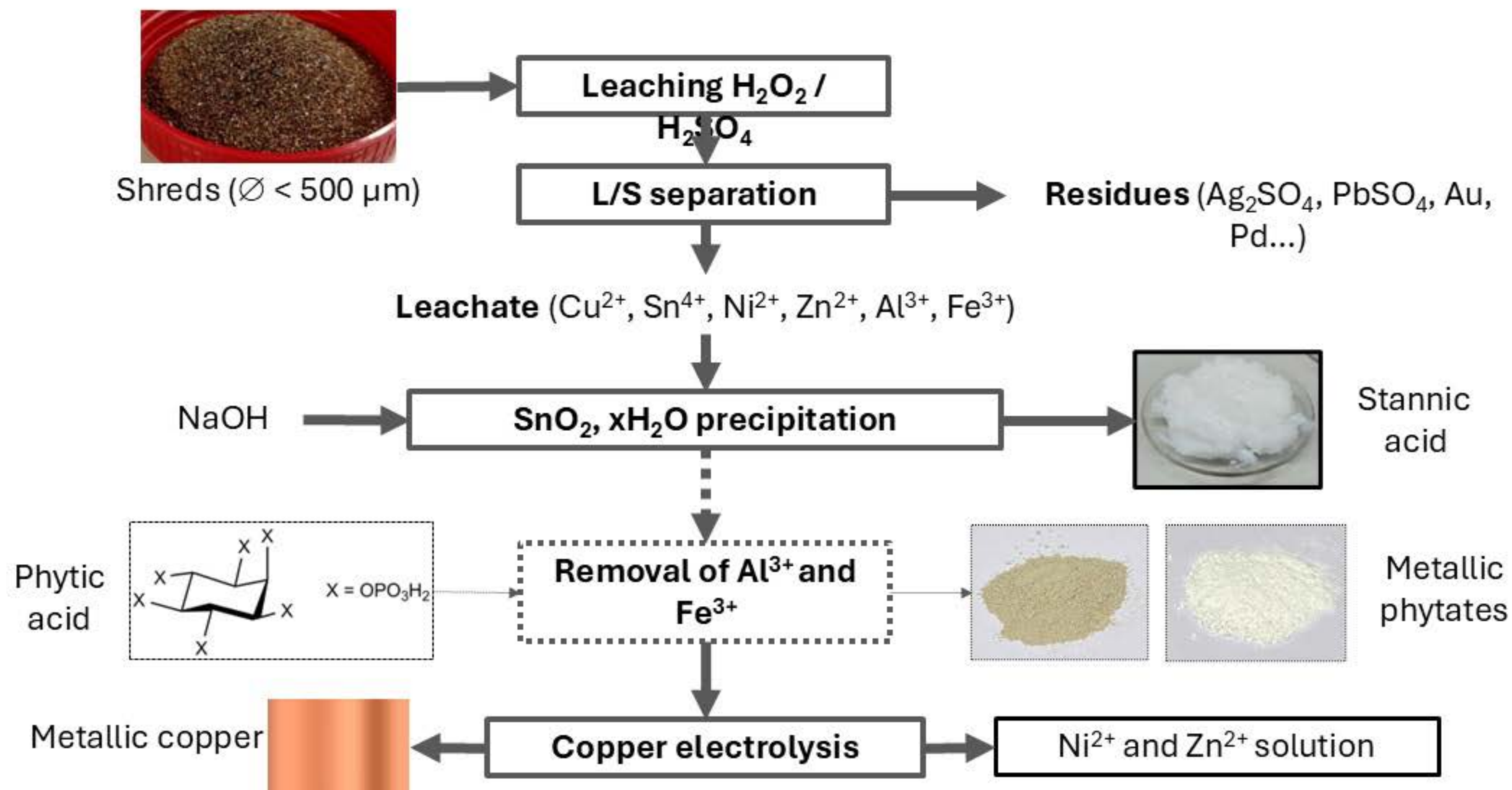
## Characterization protocol



## PCB shred composition

| Metals | Weight fraction (%) |
|--------|---------------------|
| Cu     | 52-70               |
| Sn     | 7-15                |
| Ni     | 2-4                 |
| Al     | 0.2-1.2             |
| Fe     | 0.9-1.8             |
| Zn     | 0.2-1.6             |
| Pb     | 0.1-1               |
| Ag     | 0.03-0.2            |
| Au     | 0.1-0.15            |
| Pd     | < 0.05              |

90 % of market  
value

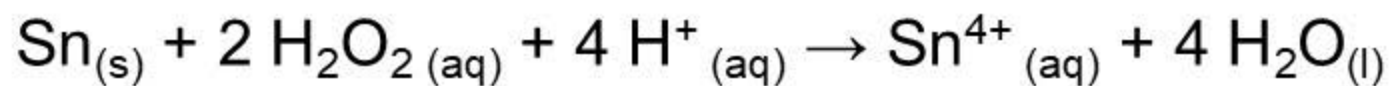
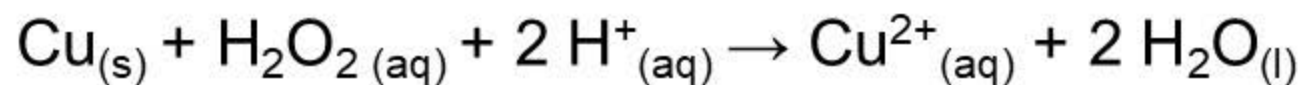




Leaching step

## Reagents

$\text{H}_2\text{O}_2\text{-H}_2\text{SO}_4$  ( $\text{H}_2\text{O}_2$  considered as a green oxidant)

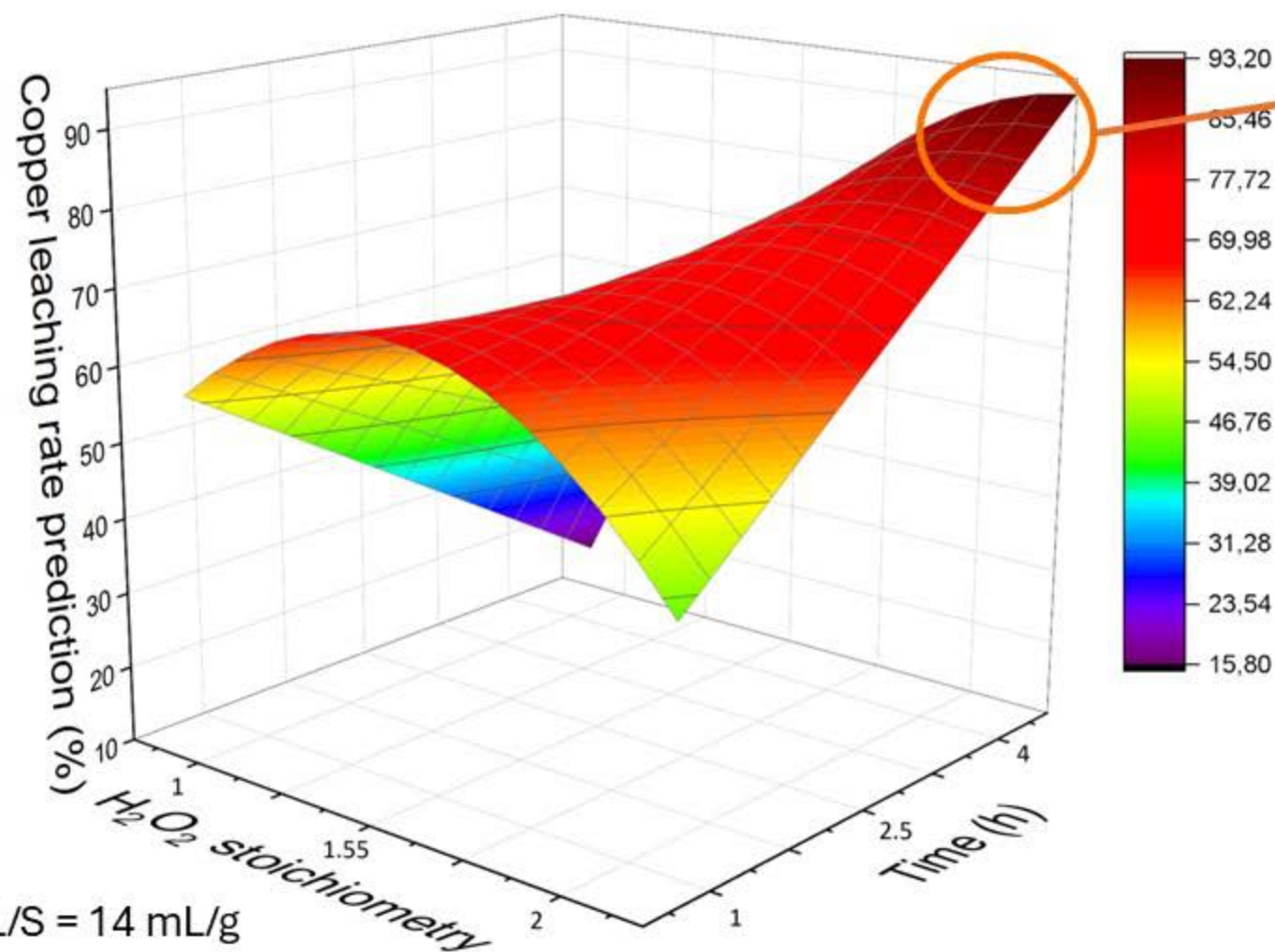


## Constraints

- Limit  $\text{H}_2\text{O}_2$  dismutation (temperature, catalysis by  $\text{Cu}^{2+}$ ,  $\text{Fe}^{2+}$ ,  $\text{Fe}^{3+}$ )
- Avoid  $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$  precipitation (solubility of 207 g/L in water at 20°C)
- Avoid prematured precipitation of  $\text{SnO}_2 \cdot x \text{H}_2\text{O}$

## Optimization – Design of Experiments

Fractional factorial design  $2^{4-1}$  then central composite design



### Optimal conditions

$$n H_2O_2 / \Sigma n \text{ métaux} = 2$$

$$n H^+ / \Sigma n \text{ métaux} = 6$$

Leaching time = 4h

Liquid/Solid ratio = 14 mL/g

Cryostat set at 20°C

Stirring rate = 300 rpm

Tested on 3 leachings

Copper leaching rate : **82.8 ± 4.4 %**

Tin leaching rate: **96.1 ± 0.5 %**

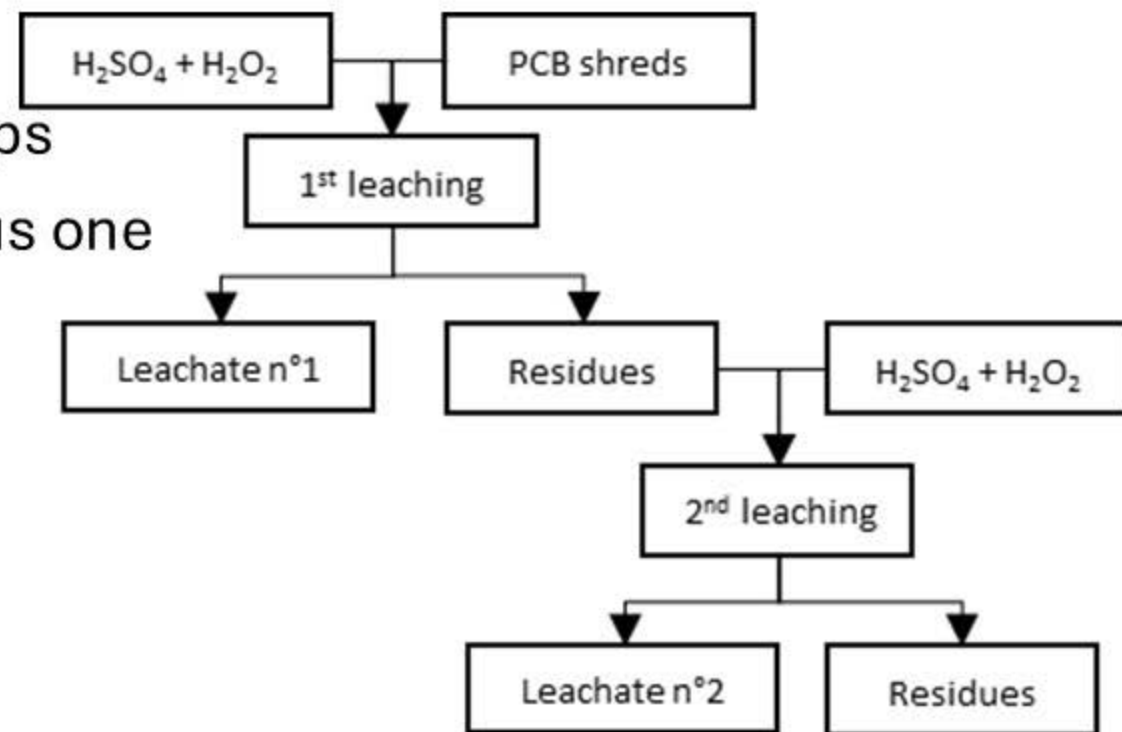
## Optimization – Multi-step leaching

$H_2O_2$  quantity divided between 2 leaching steps

Second leaching on residues from the previous one

### 3 protocols were studied

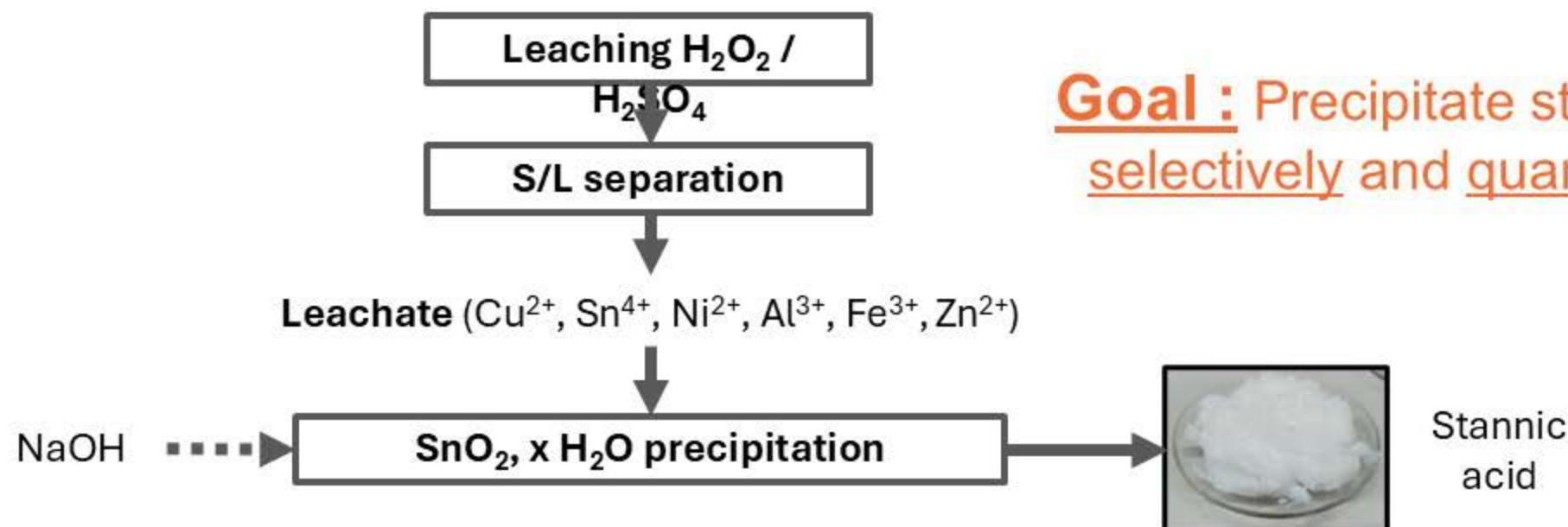
- 1-step leaching with 100 %  $H_2O_2$
- 2-steps leaching 50-50 %  $H_2O_2$
- 2-steps leaching 75-25 %  $H_2O_2$



| Leaching protocol              | One step:<br>100% $H_2O_2$ | 1 <sup>st</sup> step: 50% $H_2O_2$<br>2 <sup>nd</sup> step: 50% $H_2O_2$ | 1 <sup>st</sup> step: 75% $H_2O_2$<br>2 <sup>nd</sup> step: 25% $H_2O_2$ |
|--------------------------------|----------------------------|--------------------------------------------------------------------------|--------------------------------------------------------------------------|
| Final copper leaching rate (%) | 82.8 ± 4.4                 | 97.3 ± 1.1                                                               | 95.9 ± 2.2                                                               |
| Final tin leaching rate (%)    | 96.2 ± 0.5                 | 97.8 ± 0.2                                                               | 97.6 ± 0.3                                                               |



Recovery of tin

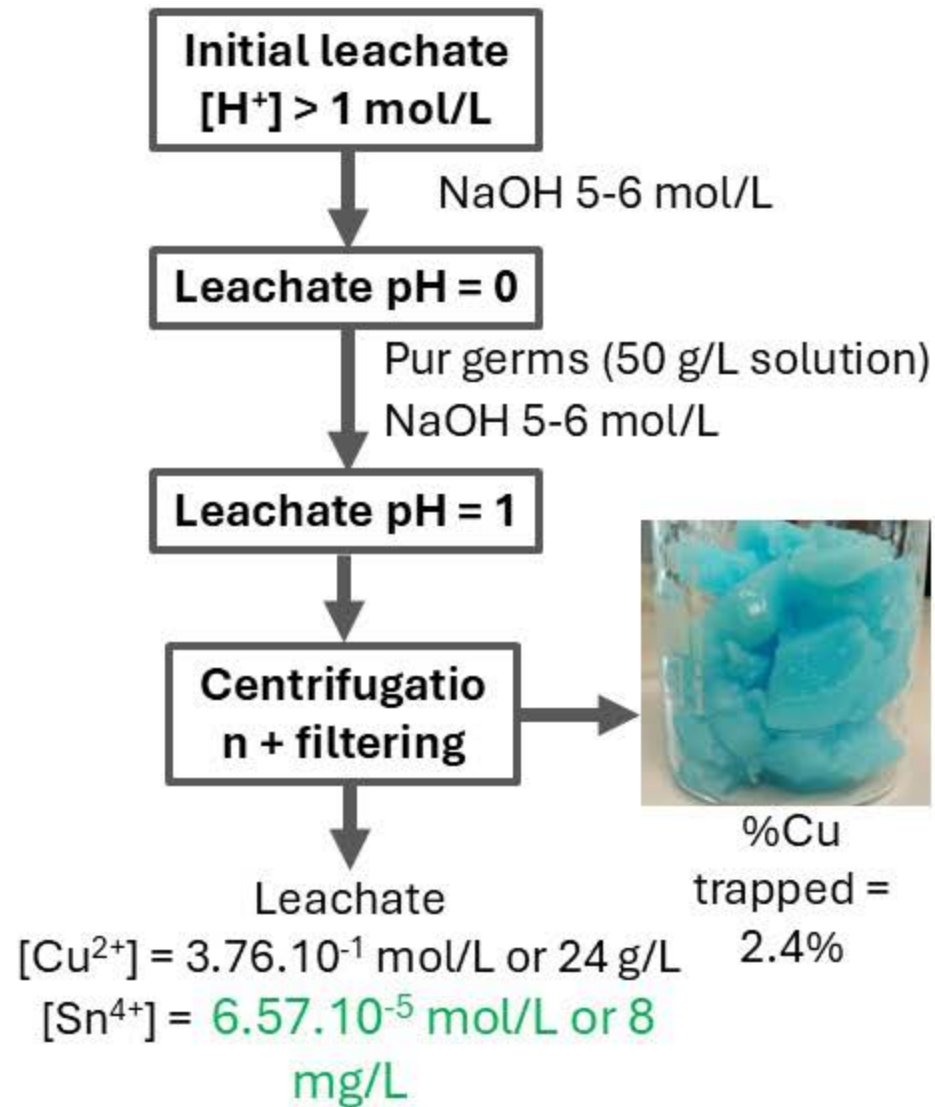


## Problems :

- Spontaneous precipitation of stannic acid at  $\text{pH} \simeq 0.3 - 0.5$ 
  - Important increase of pH → may decrease purity (goethite precipitation,  $\text{Cu}^{2+}$  adsorption)
- Precipitation delay
  - Crystal seeding at lower pH → requires pre-made stannic acid



## Crystal seeding



Washing by repulping: 1 mL H<sub>2</sub>SO<sub>4</sub> 0,1 M per gram of precipitate

Washing 1



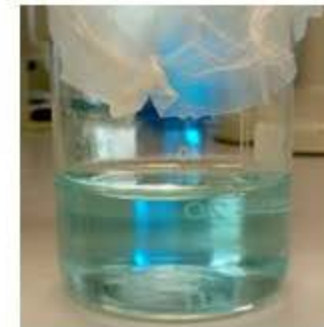
[Cu<sup>2+</sup>] =  $1.72 \cdot 10^{-1}$  mol/L  
%Cu trapped = 1,8 %

Washing 2



[Cu<sup>2+</sup>] =  $7.96 \cdot 10^{-2}$  mol/L  
%Cu trapped = 1.4 %

Washing 3

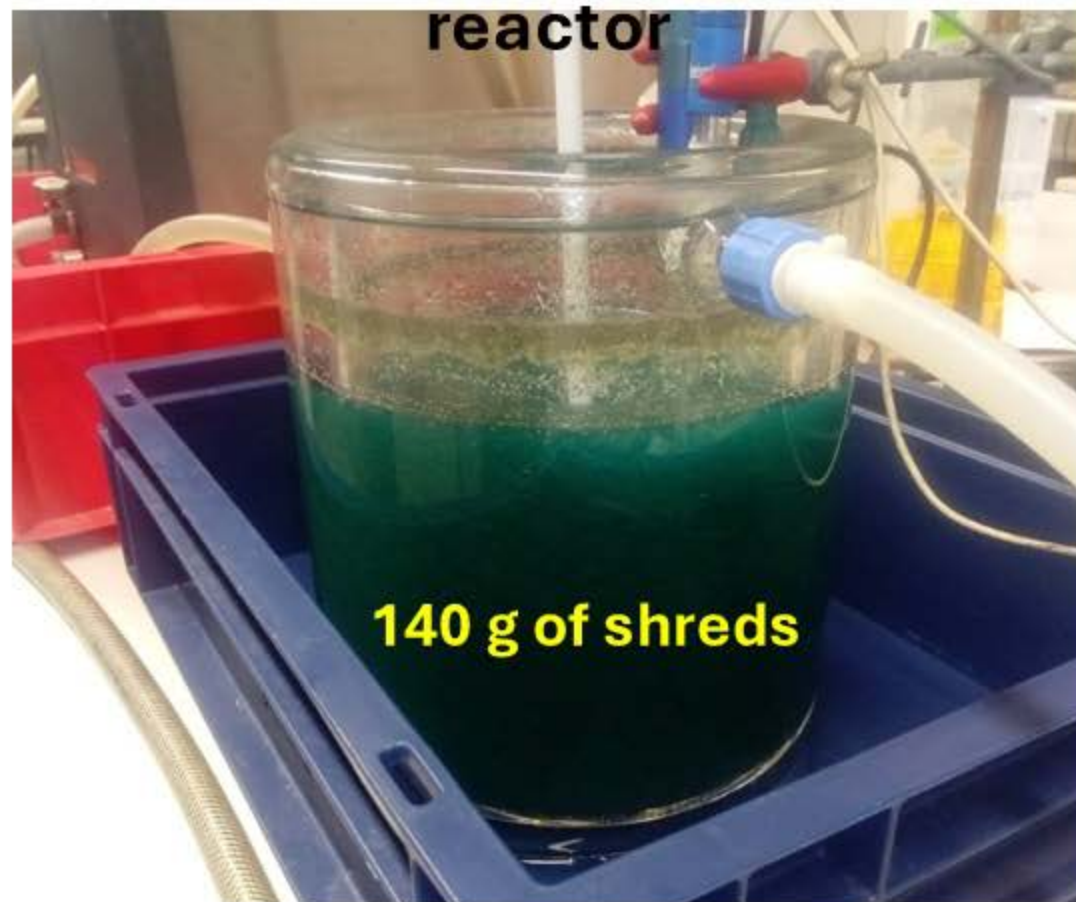


[Cu<sup>2+</sup>] =  $4.94 \cdot 10^{-2}$  mol/L  
**%Cu trapped = 1.1 %**



Scale-up

### Two-step leaching in optimal conditions in a 3 L reactor



### Optimal conditions

$n \text{ H}_2\text{O}_2 / \Sigma n \text{ métaux} = 2$  (50-50)

$n \text{ H}^+ / \Sigma n \text{ métaux} = 6$

Leaching time = 4 h

Liquid/Solid ratio = 14 mL/g

Cryostat set at 20°C

Stirring rate = 300 rpm

### Leachates gathered into

| Metal s | Concentration (g/L) | Concentration (mol/L) | Leaching rate (%) |
|---------|---------------------|-----------------------|-------------------|
| Cu      | 37.93               | $5.97 \cdot 10^{-1}$  | > 95              |
| Sn      | 5.63                | $4.8 \cdot 10^{-2}$   | > 95              |
| Ni      | 0.83                | $1.4 \cdot 10^{-2}$   |                   |
| Zn      | 0.49                | $7.5 \cdot 10^{-3}$   |                   |
| Fe      | 0.17                | $3.0 \cdot 10^{-3}$   |                   |
| Al      | 0.02                | $7.4 \cdot 10^{-4}$   |                   |

BEFOR



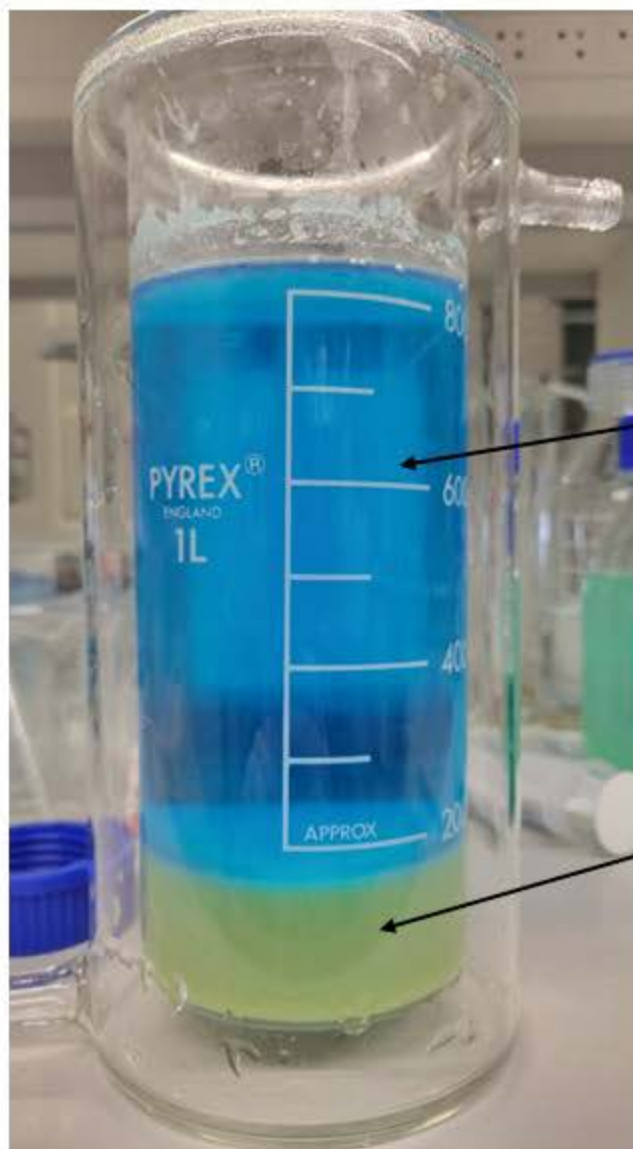
Mass loss  $\simeq 82\%$

AFTER



| Metals           | Cu   | Sn   | Ni  | Zn   | Fe   |
|------------------|------|------|-----|------|------|
| Mass content (%) | 69.3 | 12.2 | 2.6 | 1.6  | 0.9  |
| Metals           | Al   | Pb   | Ag  | Au   | Pd   |
| Mass content (%) | 0.2  | 0.9  | 0.2 | 0.09 | 0.05 |

| Metals           | Cu   | Sn  | Ni  | Zn   | Fe   |
|------------------|------|-----|-----|------|------|
| Mass content (%) | 21.2 | 2.6 | 6.4 | 0.6  | 5.5  |
| Metals           | Al   | Pb  | Ag  | Au   | Pd   |
| Mass content (%) | 0.6  | 5.7 | 1.1 | 0.26 | 0.17 |



Best results at pH = 2.5

| Metal s | Concentration (g/L) | Concentration (mol/L) |
|---------|---------------------|-----------------------|
| Cu      | 23.21               | $3.65 \cdot 10^{-1}$  |
| Sn      | 0.10                | $8.4 \cdot 10^{-4}$   |
| Ni      | 0.46                | $7.8 \cdot 10^{-3}$   |
| Zn      | 0.29                | $4.4 \cdot 10^{-3}$   |
| Fe      | 0.10                | $1.8 \cdot 10^{-3}$   |
| Al      | < 0.01              | < $3.7 \cdot 10^{-4}$ |

After 1 wash : 1% copper remaining in precipitate

Low amount of aluminum and iron  
-> **phytates precipitation step is skipped**

### Next steps :

- Copper electrolysis
- Recovery of nickel and zinc (chelating resin)

- Maximization of both copper and tin leaching from PCB shreds ( $< 500 \mu\text{m}$ ) by Design of Experiments methodology
- Savings in  $\text{H}_2\text{O}_2$  consumption with two-step leaching process
- Leaching rates of copper and tin  $> 97 \%$
- Production of a tin precipitate richer than cassiterite

$\text{SnO}_2, 2 \text{H}_2\text{O}$  (around 1% Cu trapped) represents around 70 %  $\text{SnO}_2$   
 $\Rightarrow$  production of tin via pyrometallurgy or electrolysis in alkaline medium

- **Electrolysis of copper incoming**
  - Purity of at least 99,99 % required
  - Avoid co-deposition of nickel
- **Mineralurgical characterization of leaching residues**  
(at least 100 g required)
- **Development of precious metals enrichment process** according to density, electrical conductivity, magnetic susceptibility of different phases



# Questions?





**Thank you for your  
attention**

